# An improved elasto-visco-plastic constitutive model for snow





PhD student: Gianmarco Vallero

Supervisors: Mauro Borri-Brunetto, Monica Barbero, Fabrizio Barpi XXXV cycle • PhD Programme in Civil and Environmental Engineering

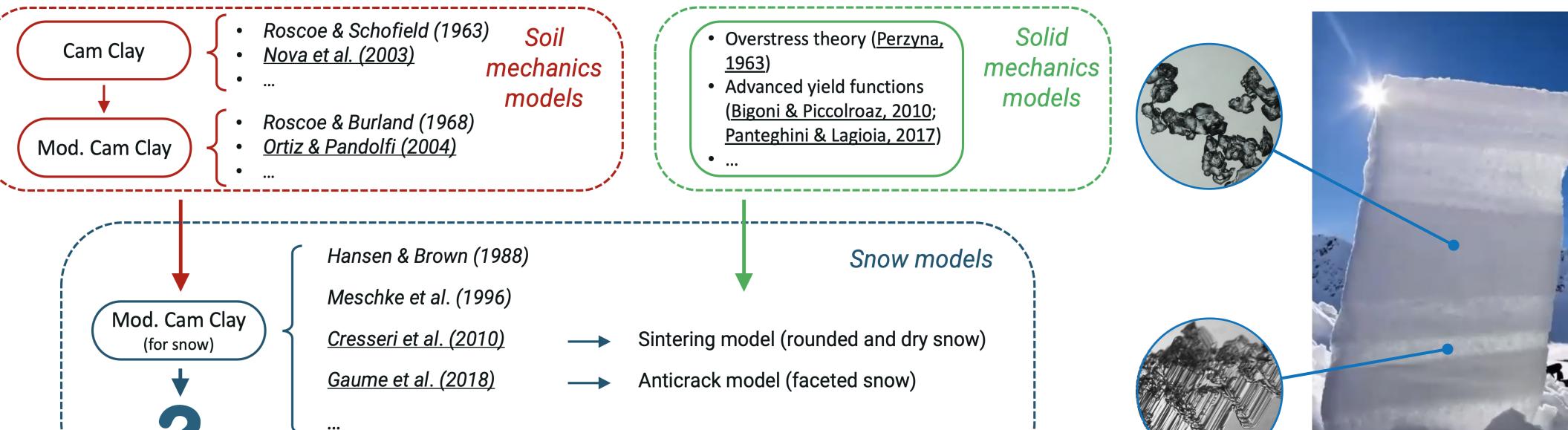
#### 1. Introduction

Snow is a granular, 3-phase, and high-porosity material whose macroscopic behaviour is strongly influenced by microstructural processes (e.g., sintering, metamorphisms and shape of grains).

Torino

Traditionally, available snow models derive from models originally conceived for soils.

For continuum mechanics purposes the Modified Cam-Clay (MCC) model is the

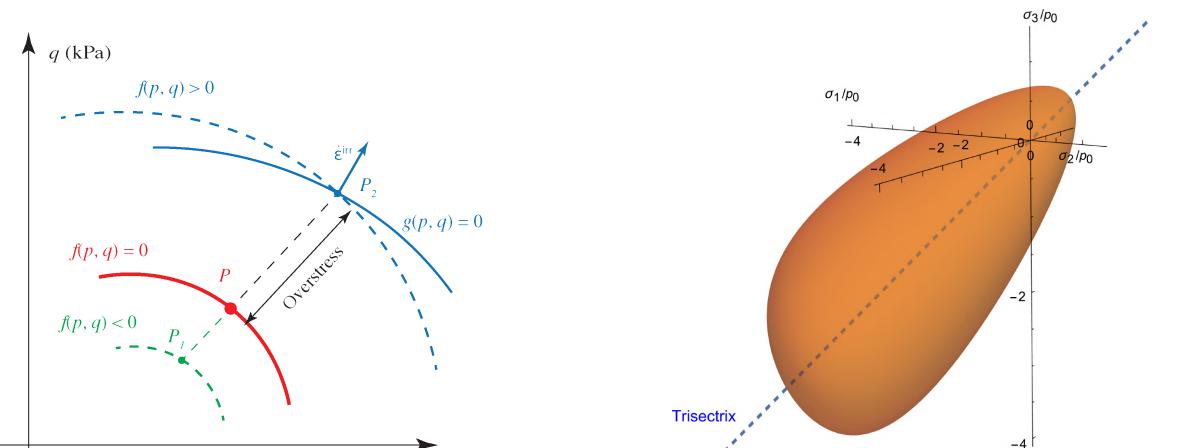


## 2. The improved model

**Initial hypotheses**: small strains, continuity, homogeneity, isotropy and isothermal conditions during the test.

- The improved model is based on three key points:
- 1. the general framework of the elasto-visco-plastic model by Cresseri et al. (2010);
- 2. the overstress theory of Perzyna (1963), accounting for irrecoverable strains even inside the elastic region;
- 3. a new formulation for an **asymmetrical yield function**.

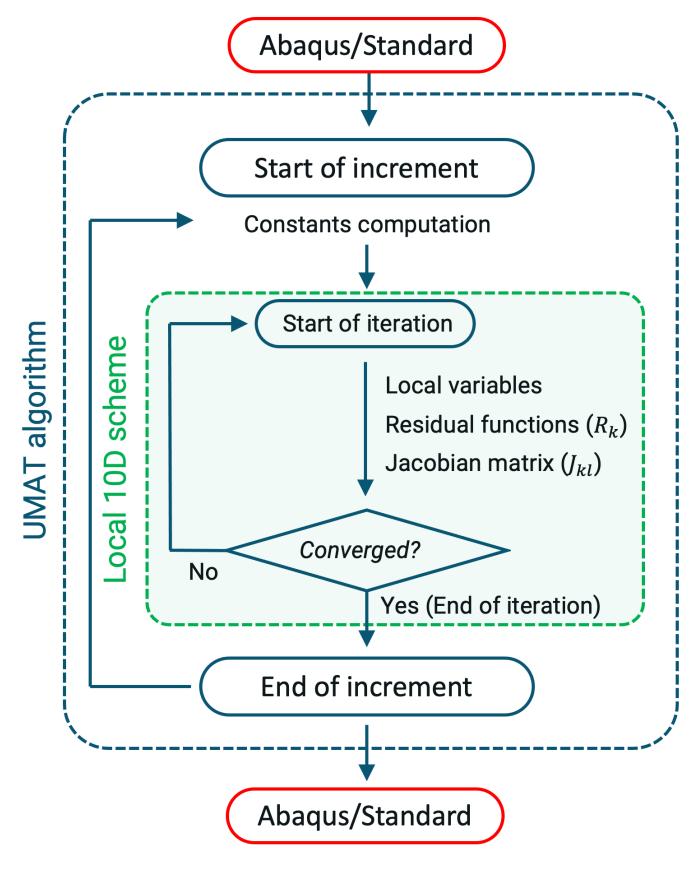
p (kPa)



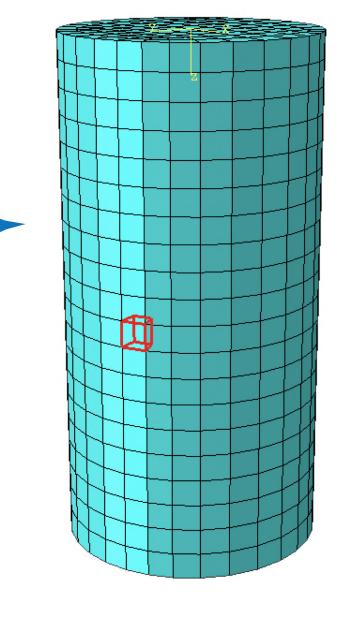
### 3. Numerical implementation

The model is time-integrated with a **fully** implicit backward Euler method.

The local problem (solving the system of 10 nonlinear differential constitutive equations) is solved with a Powel hybrid method.

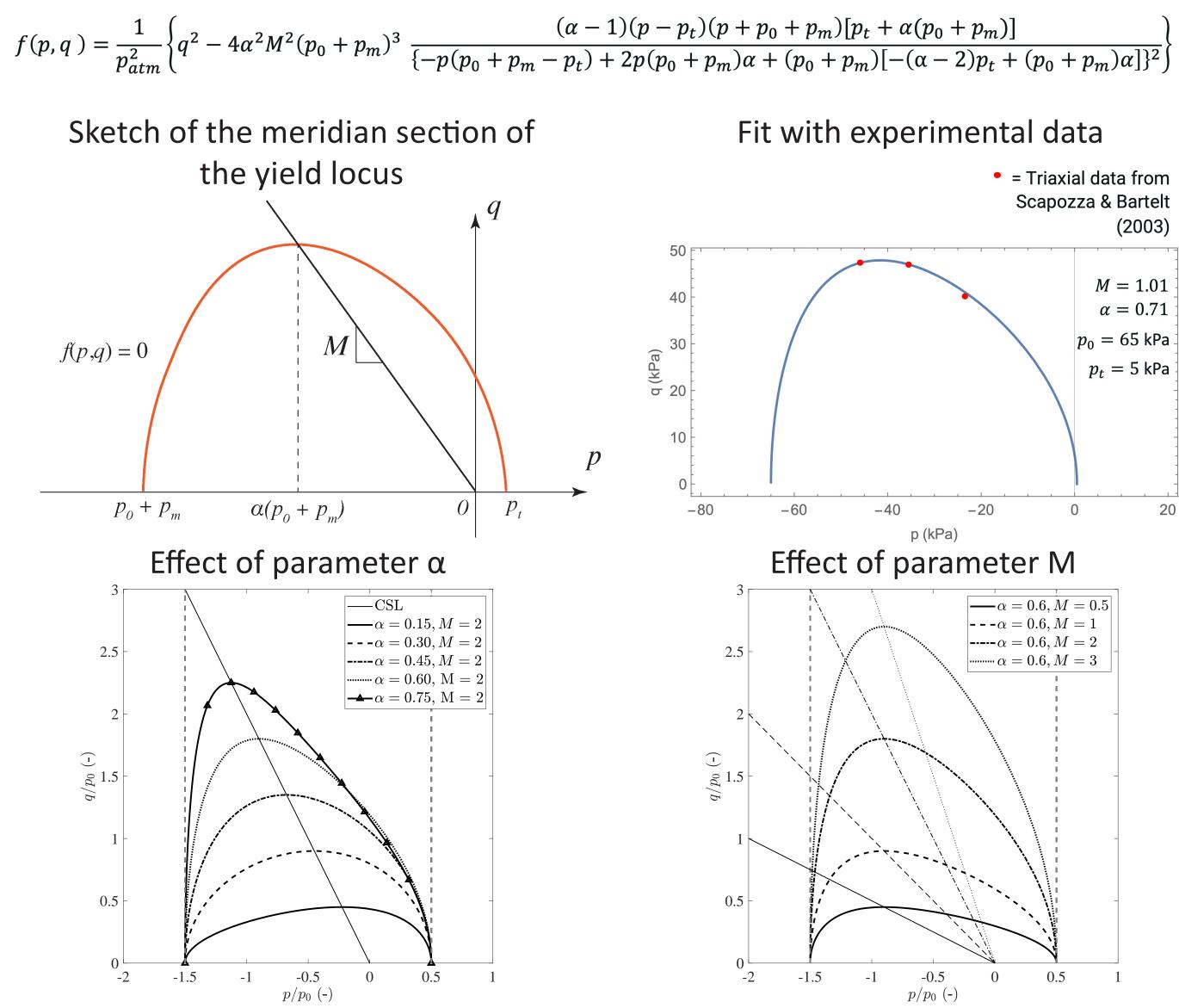


**ABAOUS** 



The model has been implemented into the **UMAT format** (Fortran 77) for the Abaqus/Standard Finite Element Code. First results were obtained with

The new yield function is introduced to account for an asymmetrical, always smooth and simply convex yield locus:



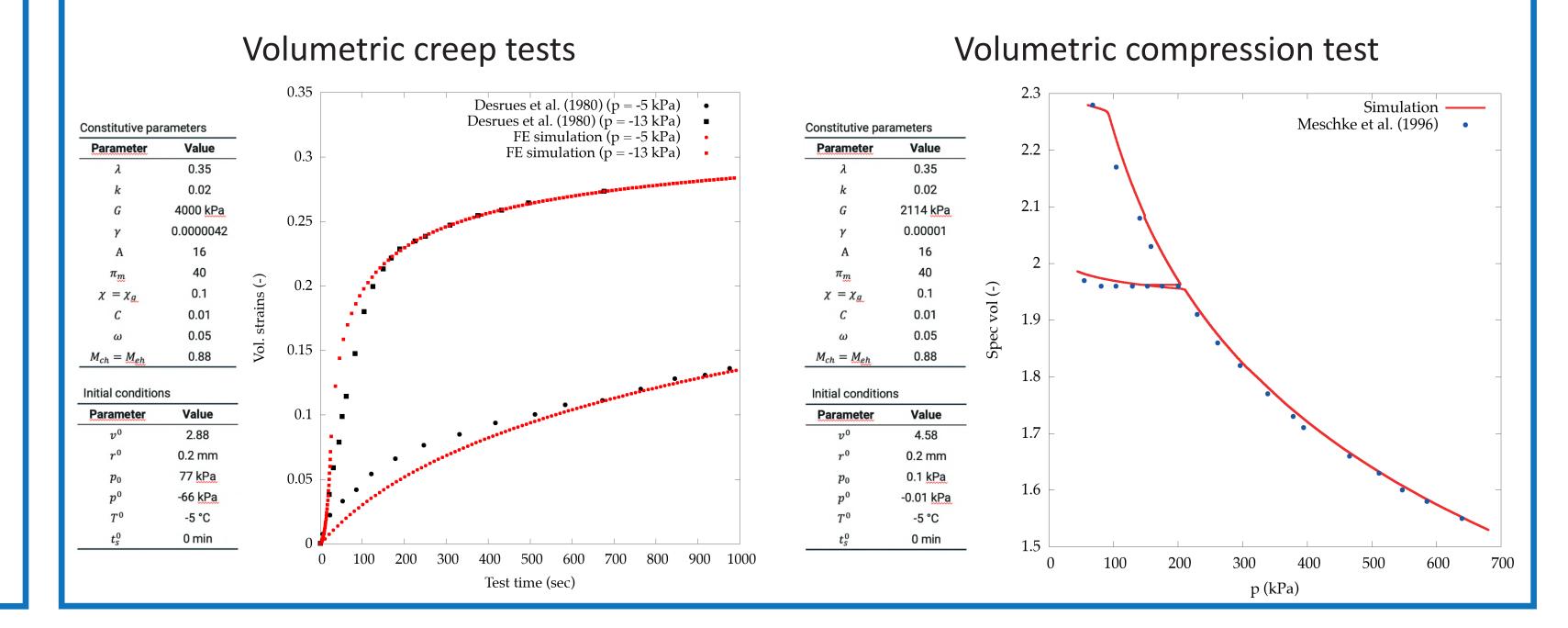
elliptical yield surface and the free code IncrementalDriver.

Local system of 10 differential constitutive equations to be solved for all time increments at any integration point:

$$\begin{split} R_{1to6} &= \frac{1}{Z_1} \left( \Delta \boldsymbol{\sigma} - \boldsymbol{D}^e(\boldsymbol{\sigma}_{n+1}) \Delta \boldsymbol{\epsilon} + \left. \boldsymbol{D}^e(\boldsymbol{\sigma}_{n+1}) \right. \beta_{n+1} \left. \frac{\partial g}{\partial \boldsymbol{\sigma}} \frac{1}{|\nabla g|} \right|_{n+1} \Delta t \right) = 0 \\ R_7 &= \frac{1}{Z_2} \left( g(\boldsymbol{\sigma}_{n+1}, p_{g0}) \right) = 0 \\ R_8 &= \frac{1}{Z_1} \left( \Delta p_0 + \frac{\boldsymbol{v}_{n+1}}{\lambda - k} (p_{0n} + \Delta p_0) \Delta \boldsymbol{\epsilon}_v^{\text{irr}} \right) = 0 \\ R_9 &= \Delta p_m - \pi_m b_{max} \Delta S = 0 \\ R_{10} &= S_n + \Delta S \\ &- \tilde{S}_0(t_s, r, T) \left\{ 1 - \tanh \left[ C \left( \sum_{i=0}^{n-1} \left( \int_{t_i}^{t_i + \Delta t_i} \sqrt{\left(\frac{\boldsymbol{\epsilon}_{v_i}^{\text{irr}}}{\Delta t_i}\right)^2} + \left(\frac{\boldsymbol{\epsilon}_{dev_i}^{\text{irr}}}{\Delta t_i}\right)^2} dt \right) + \int_{t_n}^{t_{n+1}} \sqrt{\left(\frac{\boldsymbol{\epsilon}_v^{\text{irr}}}{\Delta t}\right)^2} dt \right) \right] \right\} = 0 \end{split}$$

C ===	SUBROUTINE UMAT(STRESS,STATEV,DDSDDE,SSE,SPD,SCD, 1 RPL,DDSDDT,DRPLDE,DRPLDT,
С	<ul> <li>2 STRÁN, DSTRÁN, TIME, DTIME, TEMP, DTEMP, PREDEF, DPRED, CMNAME,</li> <li>3 NDI, NSHR, NTENS, NSTATEV, PROPS, NPROPS, COORDS, DROT, PNEWDT,</li> <li>4 CELENT, DFGRDØ, DFGRD1, NOEL, NPT, LAYER, KSPT, KSTEP, KINC)</li> </ul>
c c	INCLUDE 'ABA_PARAM.INC'
C === C	DECLARATION OF VARIABLES
	<pre>for using BLAS integer INF0,IPIV(10),LWORK(10) double precision WORK(10) double precision STRESS,STATEV,DDSDDE,SSE,SPD,SCD, 1 RPL,DDSDDT,DRPLDE,DRPLDT, 2 STRAN,DSTRAN,TIME,DTIME,TEMP,DTEMP,PREDEF,DPRED, 3 PROPS,COORDS,DROT,PNEWDT, 4 CELENT,DFGRD0,DFGRD1 double precision bmax double precision mat double precision p0 double precision s0 double precision S0 double precision S0 double precision t0Tilde</pre>
	<pre>double precision TempRatio double precision tTilde double precision, external :: YieldF double precision, external :: fBETA integer mm end claration of internal variables and constants CHARACTER*80 CMNAME DIMENSION STRESS(NTENS),STATEV(NSTATEV), 1 DDSDDE(NTENS,NTENS),DDSDDT(NTENS),DRPLDE(NTENS), 2 STRAN(NTENS),DSTRAN(NTENS),TIME(2),PREDEF(1),DPRED(1),</pre>

Some results obtained on the basis of available literature data:



Cresseri S, Genna F, Jommi C (2010) Numerical integration of an elastic-viscoplastic constitutive model for dry metamorphosed snow. Int J Num Anal Met Geomech 34(12), 1271-1296

Panteghini A & Lagioia R (2018) An extended modified Cam-Clay yield surface for arbitrary meridional and deviatoric shapes retaining full convexity and double homothety. Géotechnique 68(7), 590-601

#### Oral presentations / Publications (last year)

- Vallero G. et al. An improved asymmetrical yield surface for the elasto-visco-plastic modelling of snow (in preparation)
- Vallero G. et al. (2022) Experimental study of the shear strength of a snow-mortar interface. Cold Reg Sci Technol 193
- Vallero G. et al. (2022) Some Computational Issues in the Elasto-Plastic Modelling of Snow. Proc. of COMPLAS 2021
- Vallero G. et al. (2022) Advances in Constitutive Modelling of Snow for Finite Element Analysis. AIMETA 2022, Palermo (Italy), 4-8 September 2022
- Vallero G. et al. (2022) New perspectives for the elasto-plastic modelling of snow. WCCM-APCOM 2022, online, 31 July - 5 August 2022

## Contact



Ing. Gianmarco Vallero PhD student, Dept. DISEG Politecnico di Torino (Italy)

gianmarco.vallero@polito.it  $\square$ +39 011 090 4863